

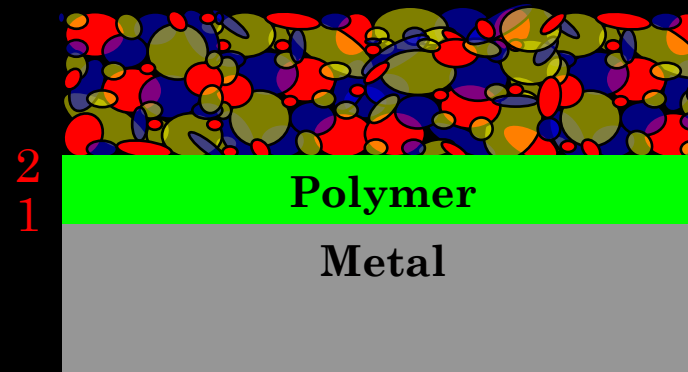
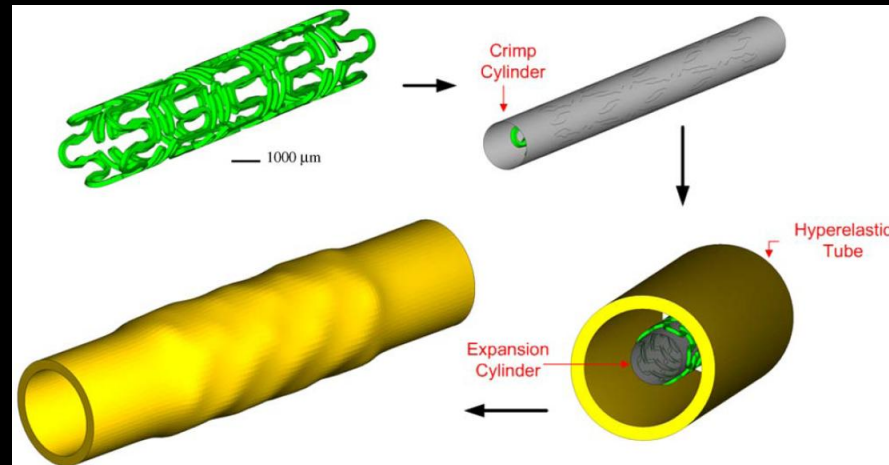


Adhesion and Interfacial Failure in Drug Eluting Stents

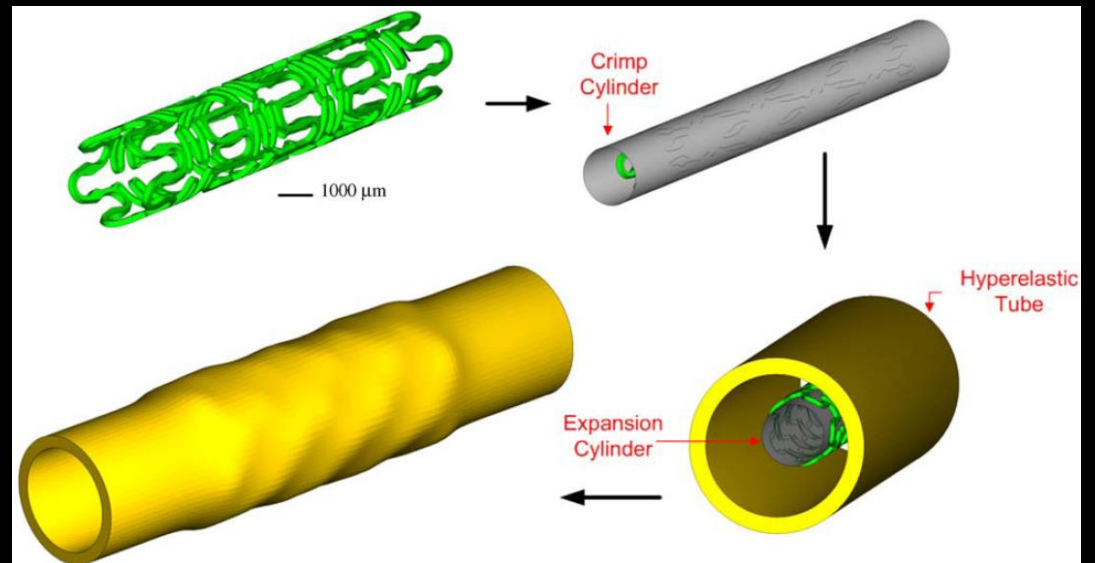
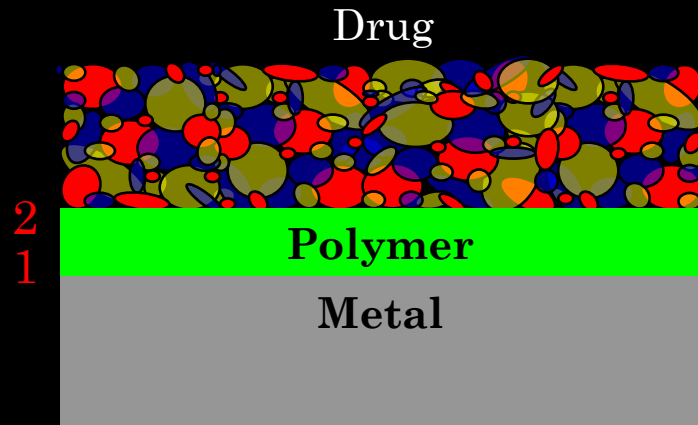
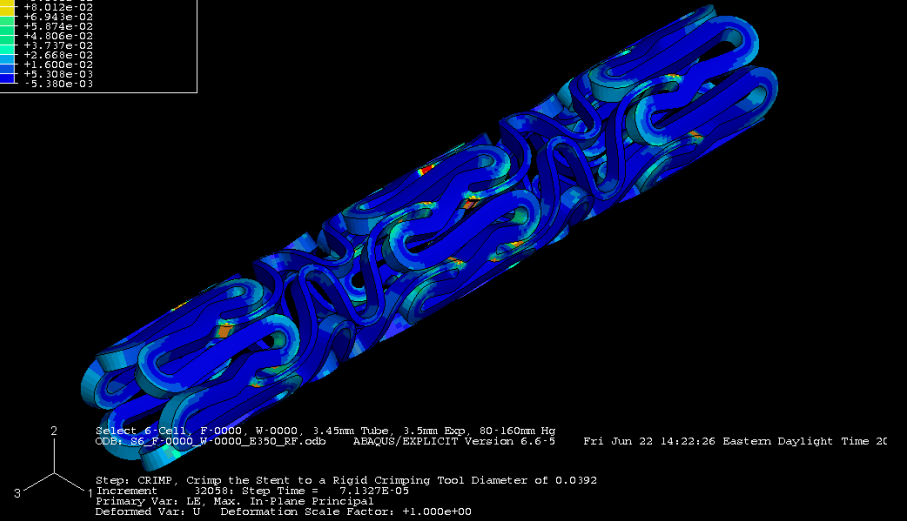
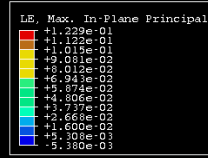
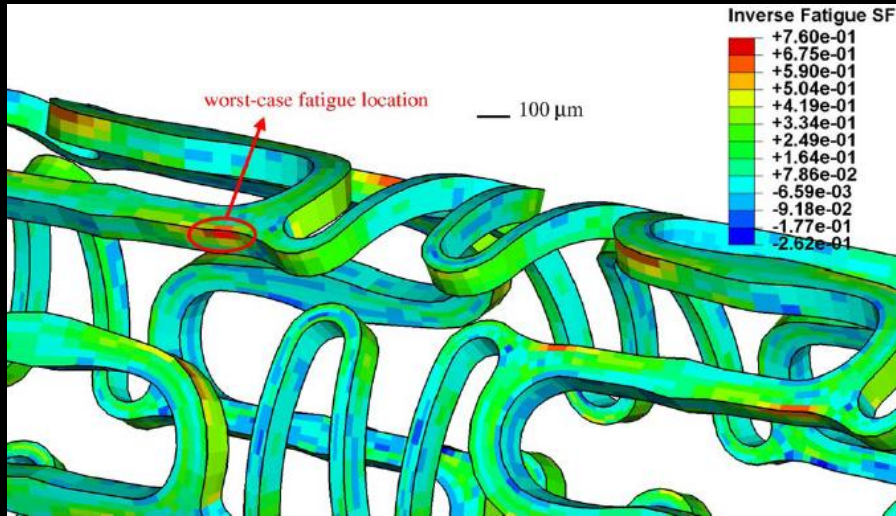
Background and Introduction



- *Cardiovascular disease is the leading cause of death across the world*
- *It represents about 30% of all deaths*
- *Stents represent a life saving technology for arteriosclerosis*
- *Drug Eluting Stents (DES) reduce the possibility of clotting after stent insertion*

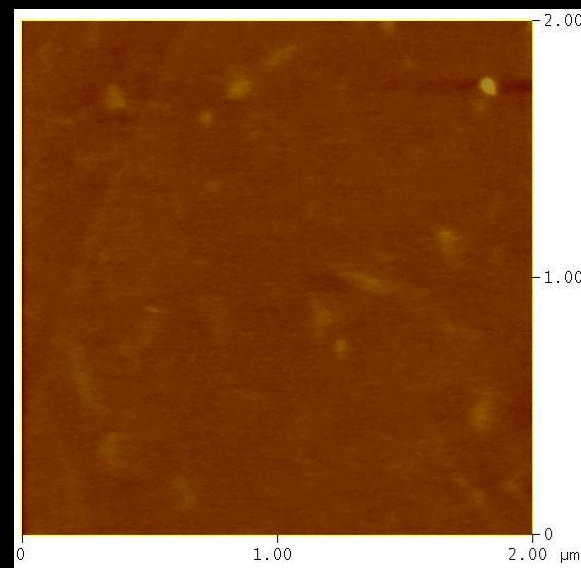
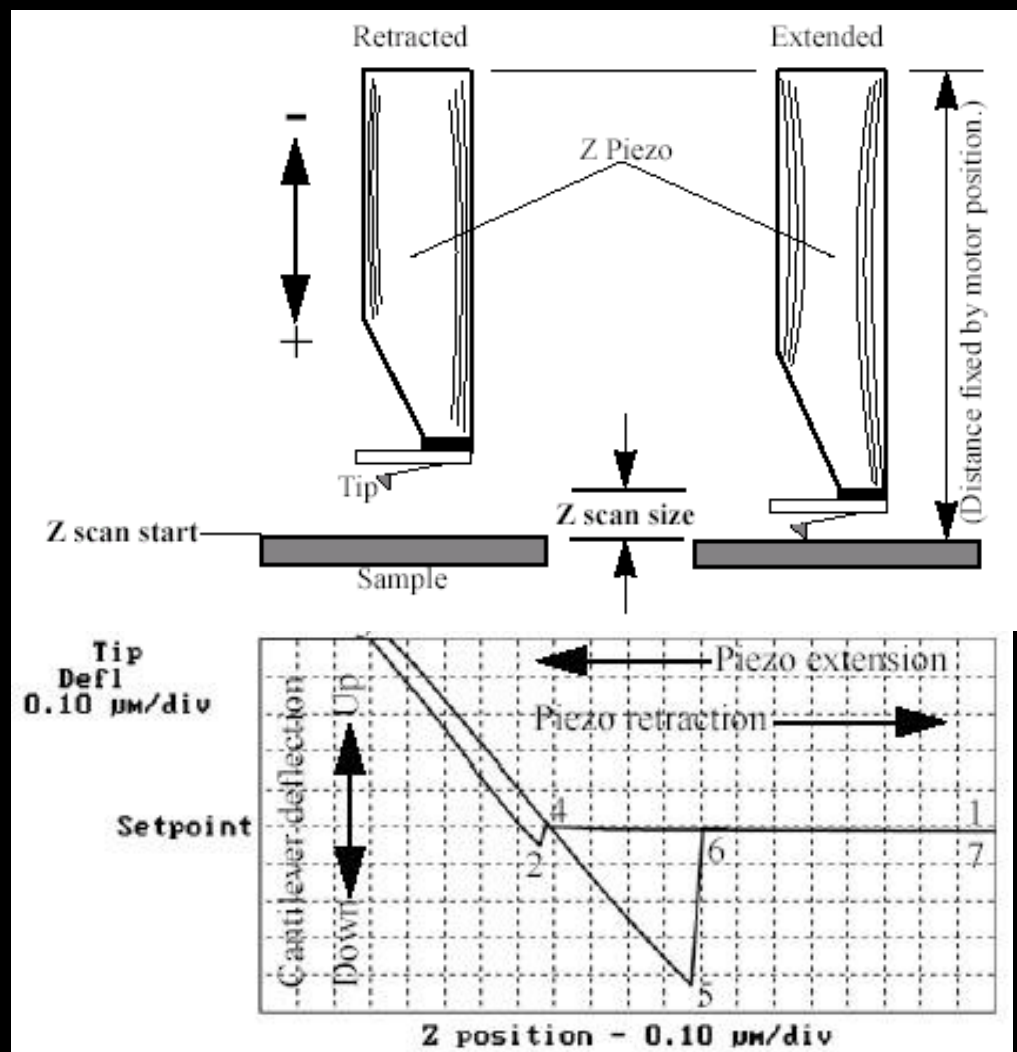


Drug-Eluting Stents

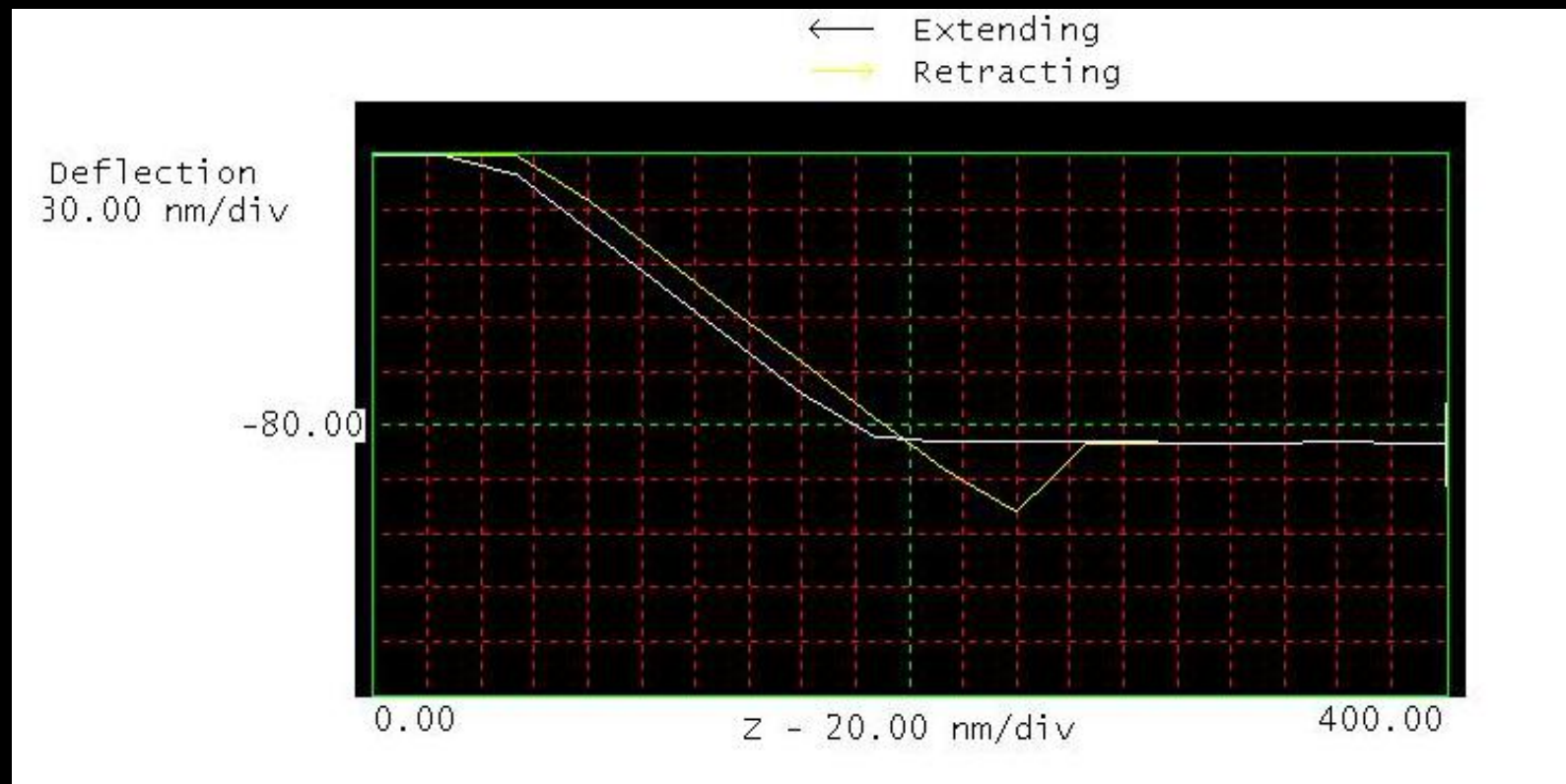


Marrey RV et al. (2006)
Biomaterials 27:1988–2000

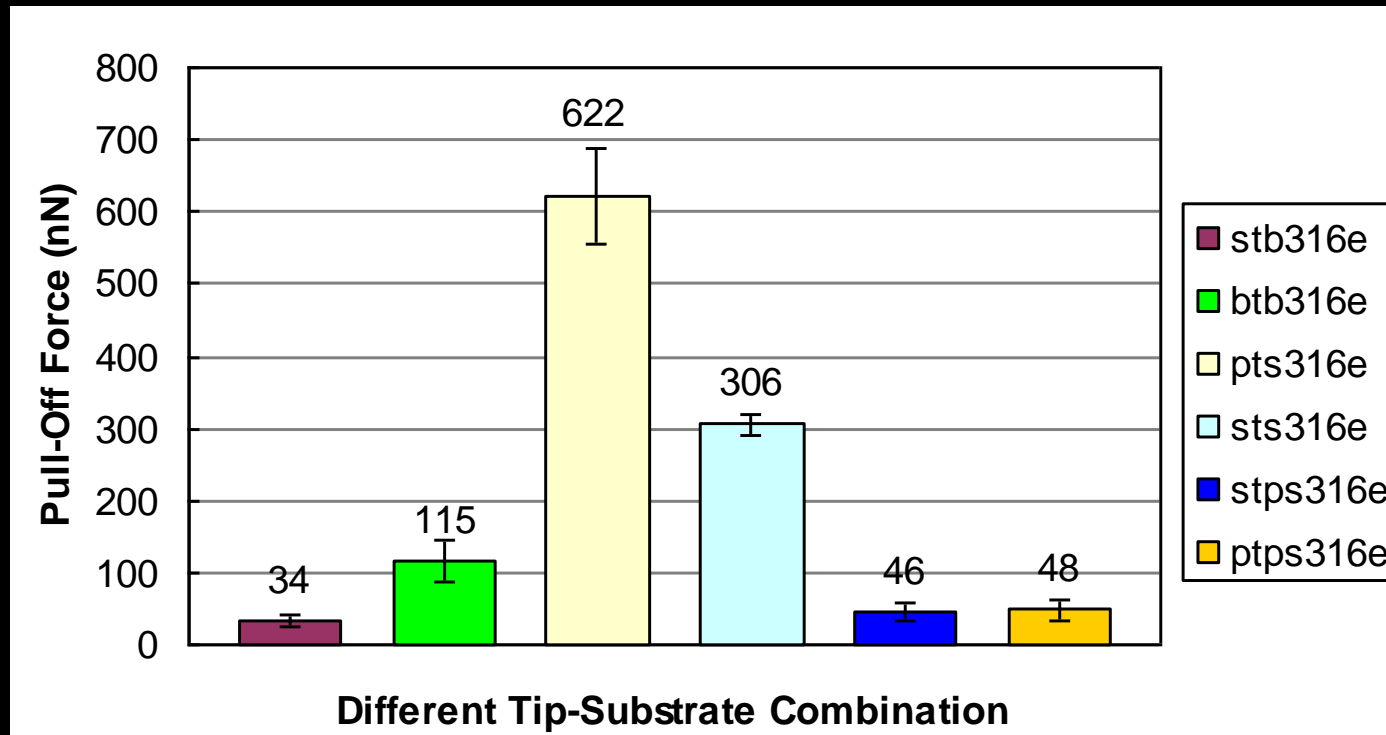
AFM Adhesion Pull-Off Force Measurement



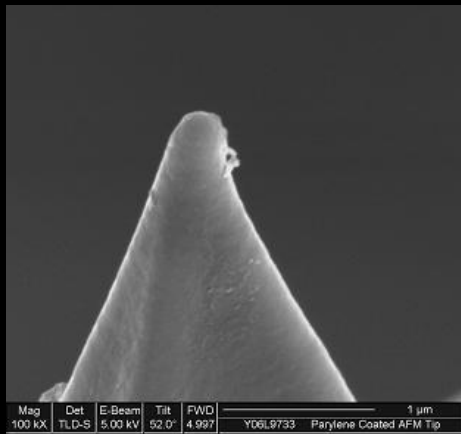
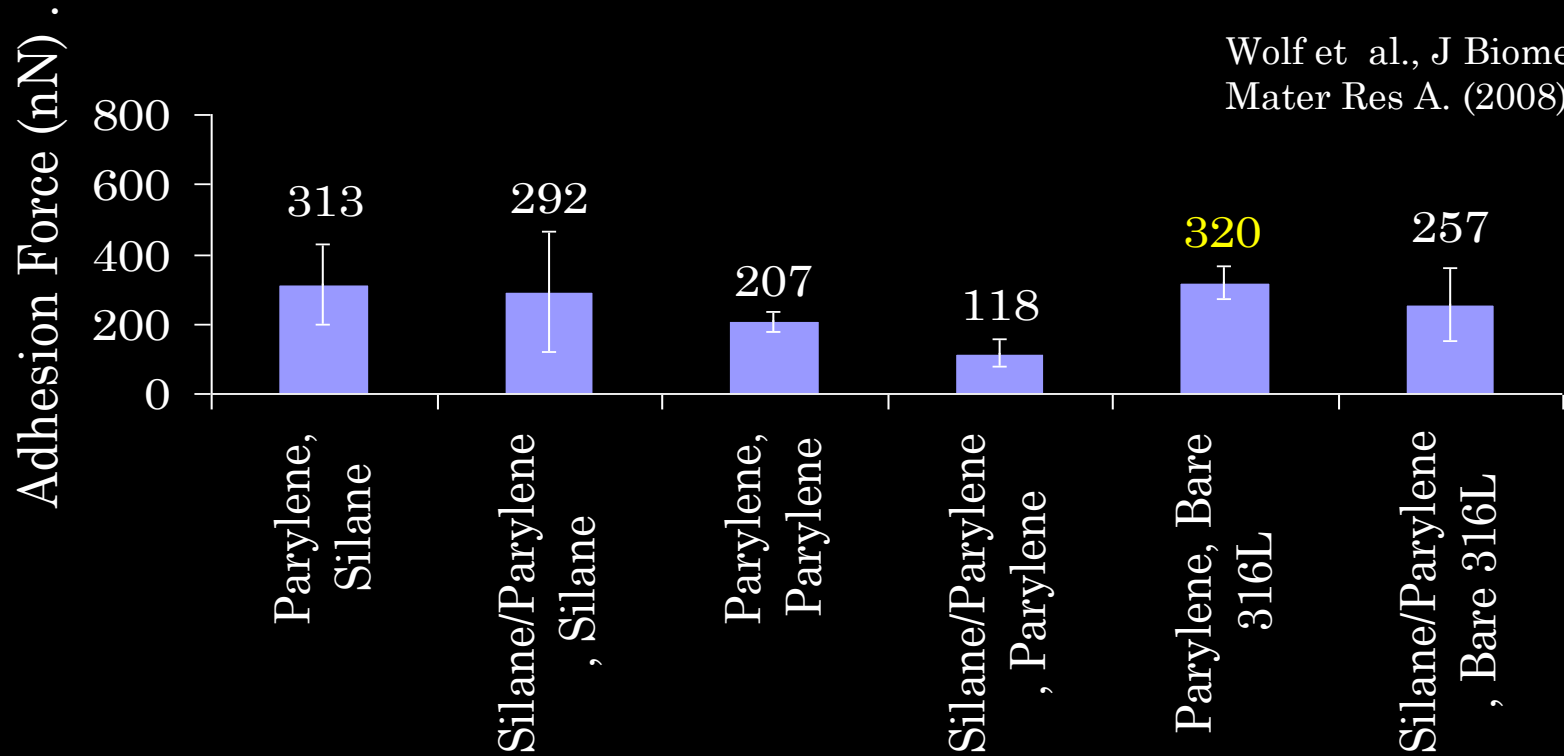
AFM Adhesion Pull-Off Force Measurement



AFM Adhesion Pull-Off Force Measurement

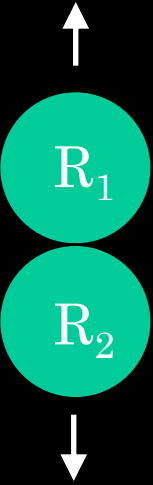


Experiments: AFM



Surface Coating	Average Coupon rms Roughness (nm)	Coupon STD (nm)
EP 316L	106	42
Surface Coating	Average Radius (nm)	Radius STD (nm)
Parylene C	370	31

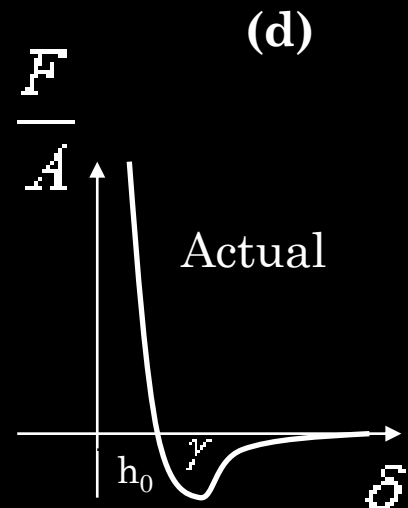
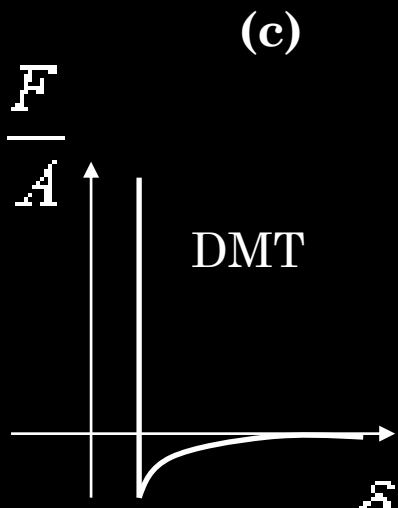
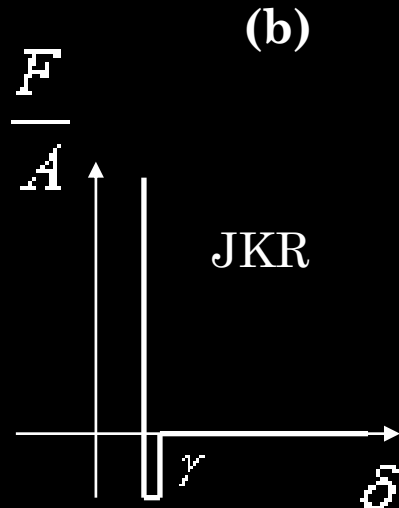
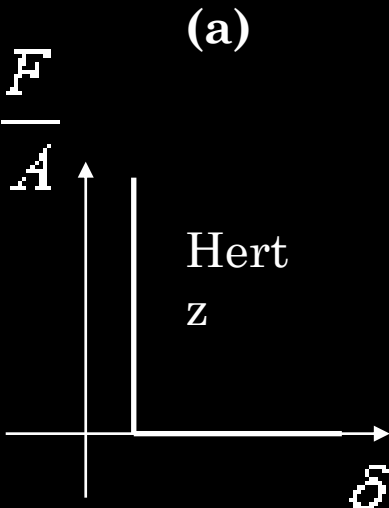
Adhesion Theory



$$F_{ad} = \bar{F} \pi \gamma R$$

$$\frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2}$$

$$\gamma = \gamma_1 + \gamma_2 - \gamma_{12}$$



Johnson KL, Kendall K, Roberts AD (1971) *Proc. R. Soc. London, Ser.A*, 324,

Derjaguin BV, Muller VM, Toporov YP (1975) *J. Colloid Interface Sci.*, 53, 314.



Adhesion Theory

Johnson–Kendall–Roberts (JKR)

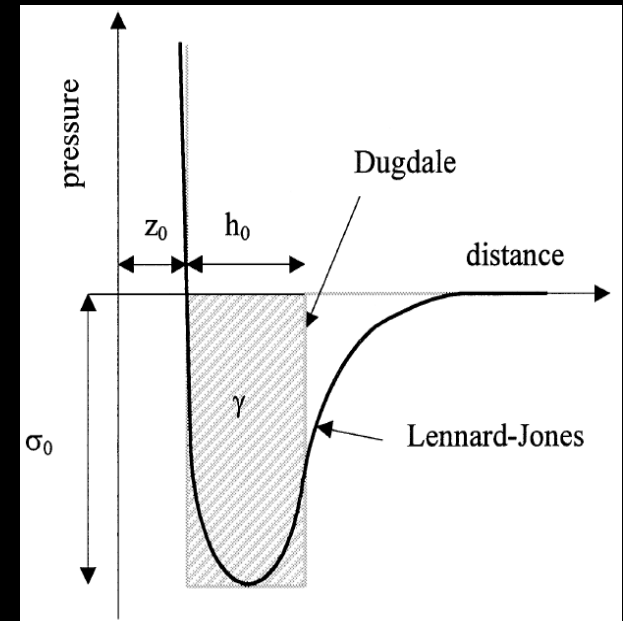
model: describes well the contact area when the surface forces are short range in comparison to the elastic deformations they produce (i.e., compliant materials, strong adhesion forces, large tip radii)

$$F_{JKR} = \frac{3}{2} \pi \gamma R$$

Derjaguin–Muller–Toporov (DMT):

applies well in the case of long-range surface forces with an hertzian geometry (i.e., stiff materials, weak adhesion forces, small tip radii)

$$F_{DMT} = 2\pi \gamma R$$



$$\lambda = 2\sigma_0 \left(\frac{R}{\pi K^2 \gamma} \right)^{1/3}$$

$$\lambda = f(\alpha) = -0.913 \ln(1 - 1.018\alpha)$$

General case

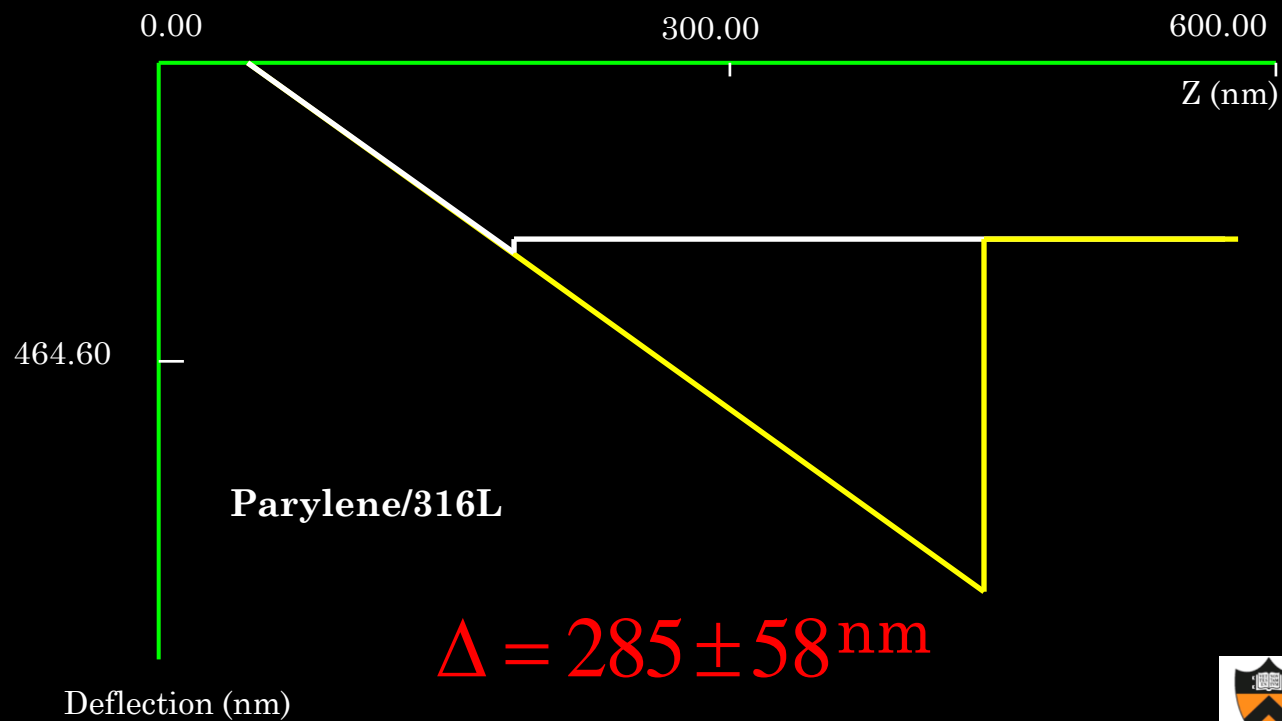
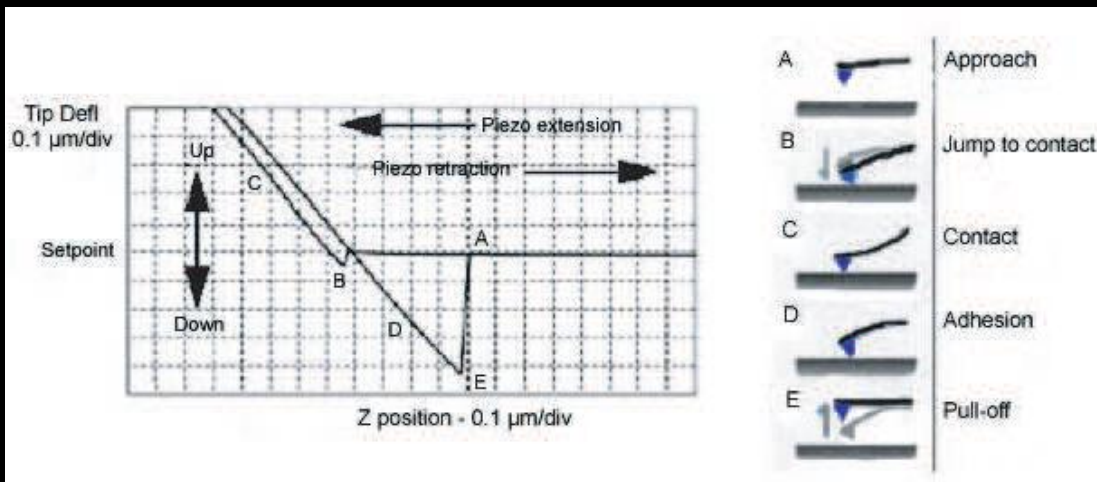
$$F_{ad} = \bar{F} \pi \gamma R$$

$$\bar{F} = 0.267\alpha^2 - 0.767\alpha + 2.000$$

$$\gamma = \sigma_0 h_0$$

Carpick RW, Ogletree DF, and Salmeron M (1999) *J. Colloid Interface Sci.*, 211, 395.

Typical Force-Displacement Curve



Modeling AFM Adhesion

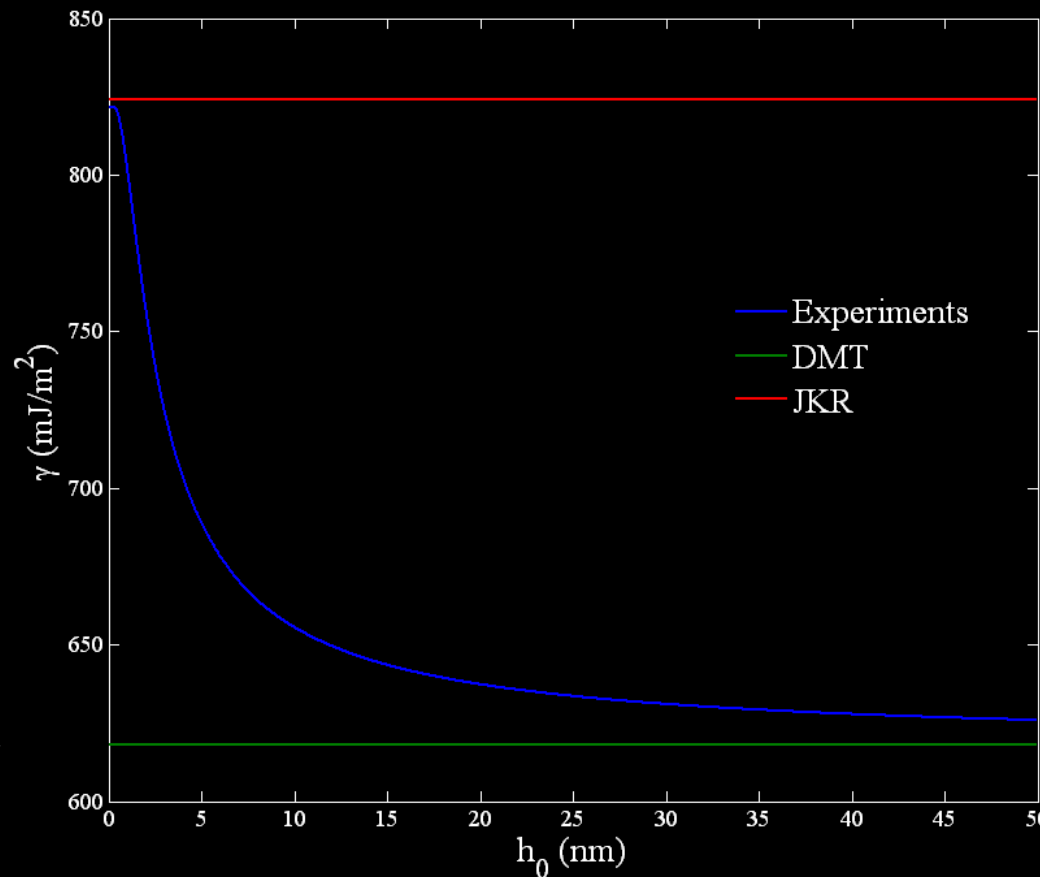
- *Parylene/316L*
Adhesion Energy:

$$\lambda = 2\sigma_0 \left(\frac{R}{\pi K^2 \gamma} \right)^{1/3}$$

$$\lambda = f(\alpha) = -0.913 \ln(1 - 1.018\alpha)$$

$$\bar{F} = 0.267\alpha^2 - 0.767\alpha + 2.000$$

$$\gamma = \sigma_0 h_0$$



$$R = 370 \text{ nm}$$

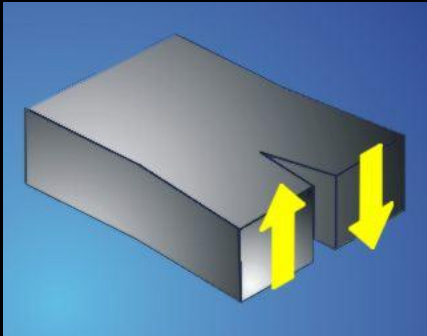
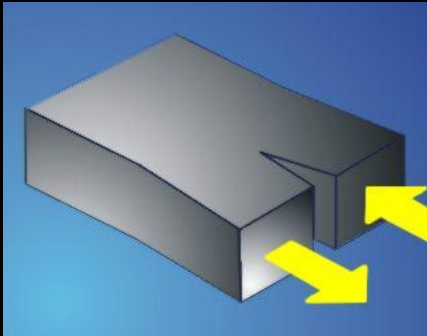
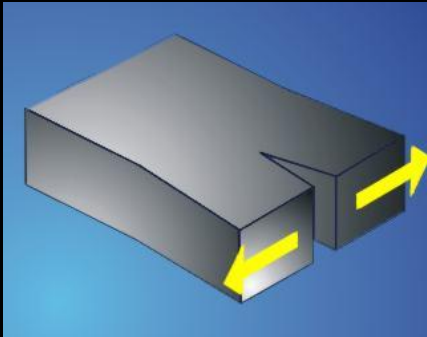
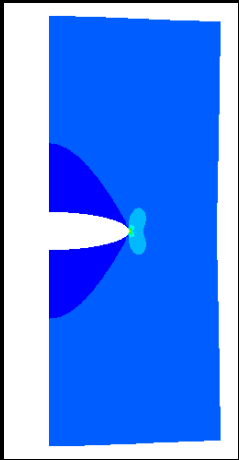
$$F_{ad} = 320 \text{ nN}$$

Lorentz–Berthelot mixing rule:

$$h_{012} = \frac{1}{2} (h_{01} + h_{02})$$



Fracture Mechanics



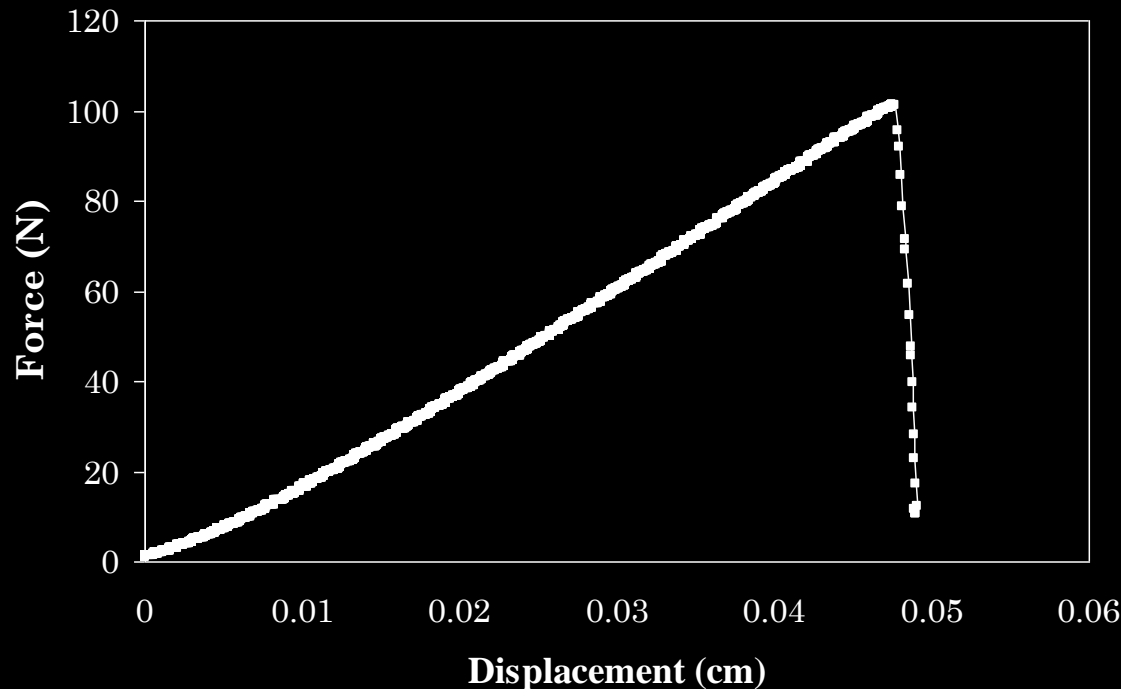
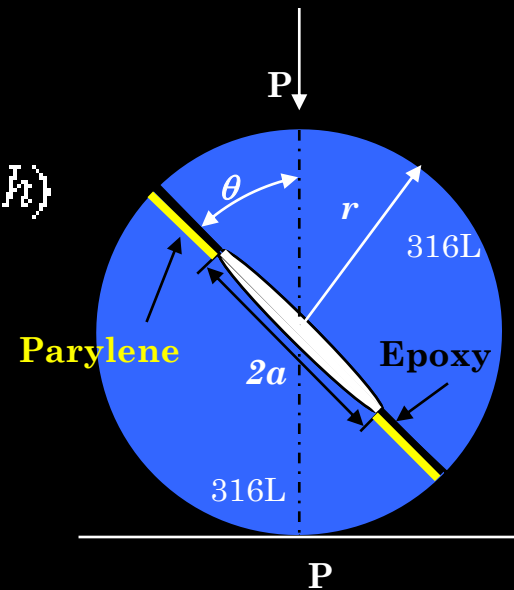
Experiments: Brazil nuts

Energy release rate: $G = \frac{1}{E'} (K_I^2 + K_{II}^2)$

Loading phase: $\psi = \tan^{-1}(K_{II}/K_I) + \omega + \varepsilon \ln(\hat{L}/h)$

$$K_I = f_I P a^{-1.2}$$

$$K_{II} = f_{II} P a^{-1.2}$$



Wang and Suo, *Acta Metall. Mater.*, 38 (7): 1279-1290;

Atkinson et al., *Int J Fract Mech* 18 (4): 279-291.

Typical Fracture Surfaces: Parylene/Steel Sample #8

Figure 9 - Flat Not Marked

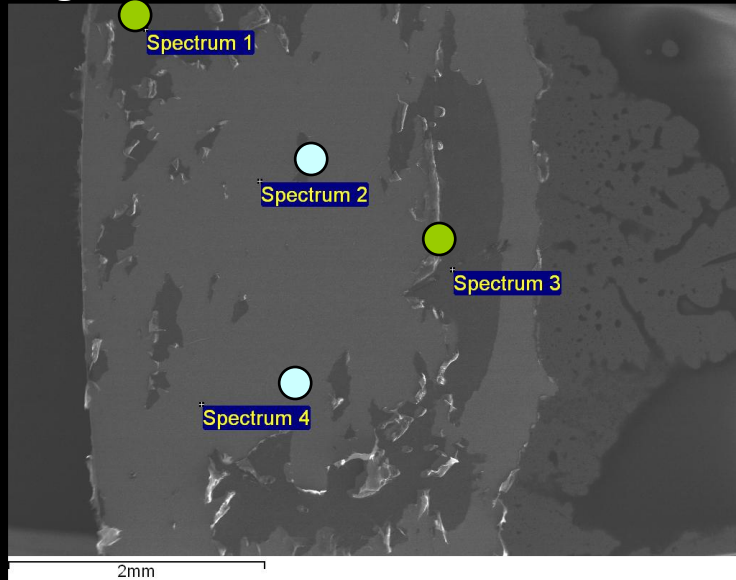


Figure 10 - Notch Not Marked

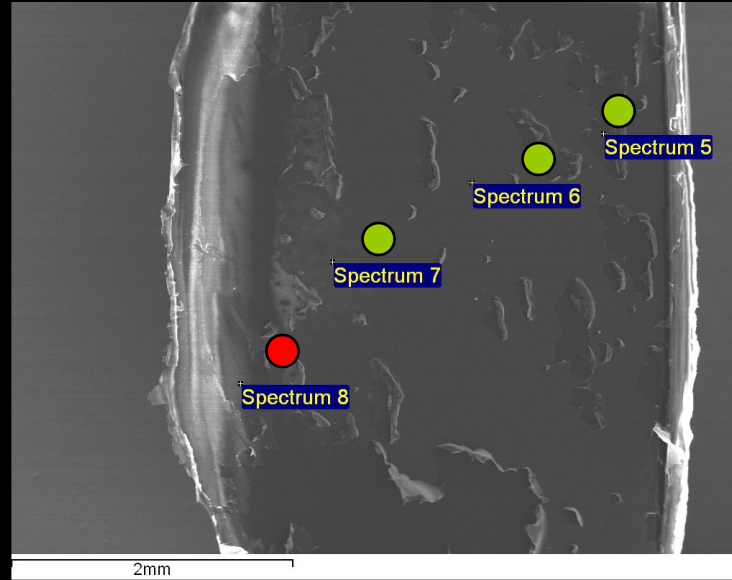


Figure 11 - Notch Marked

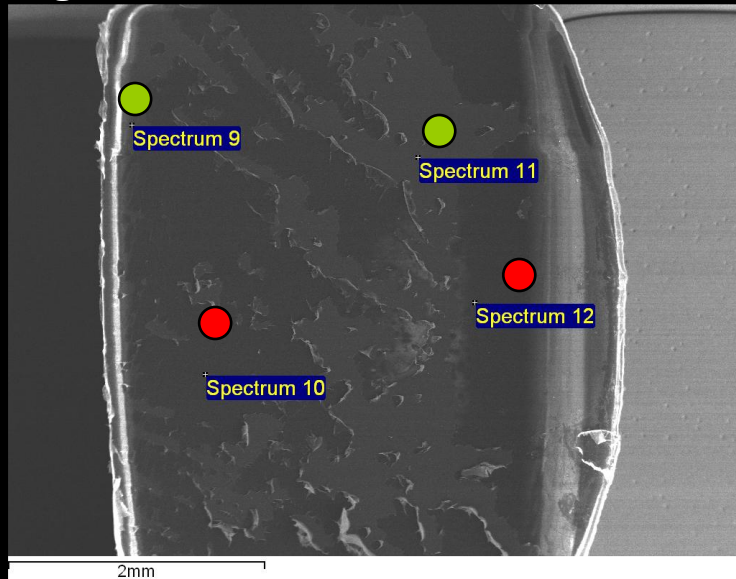
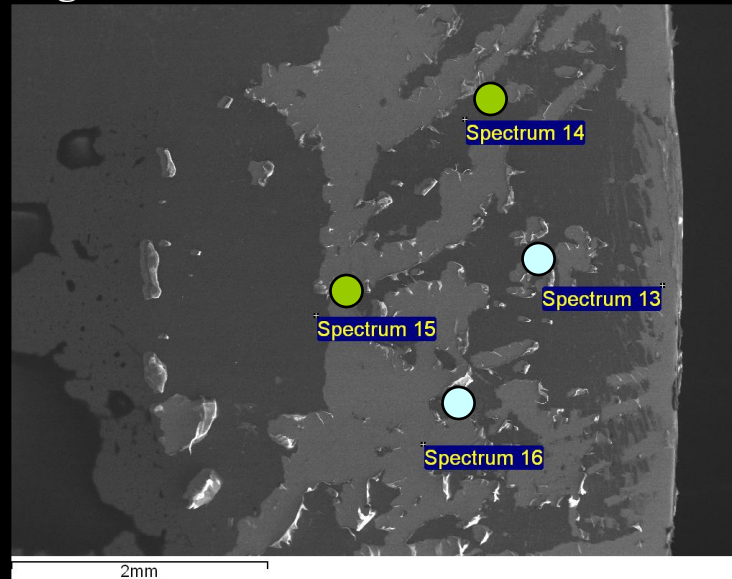


Figure 12 - Flat Marked



● **Parylene:**
Spectra
found >1%
Cl

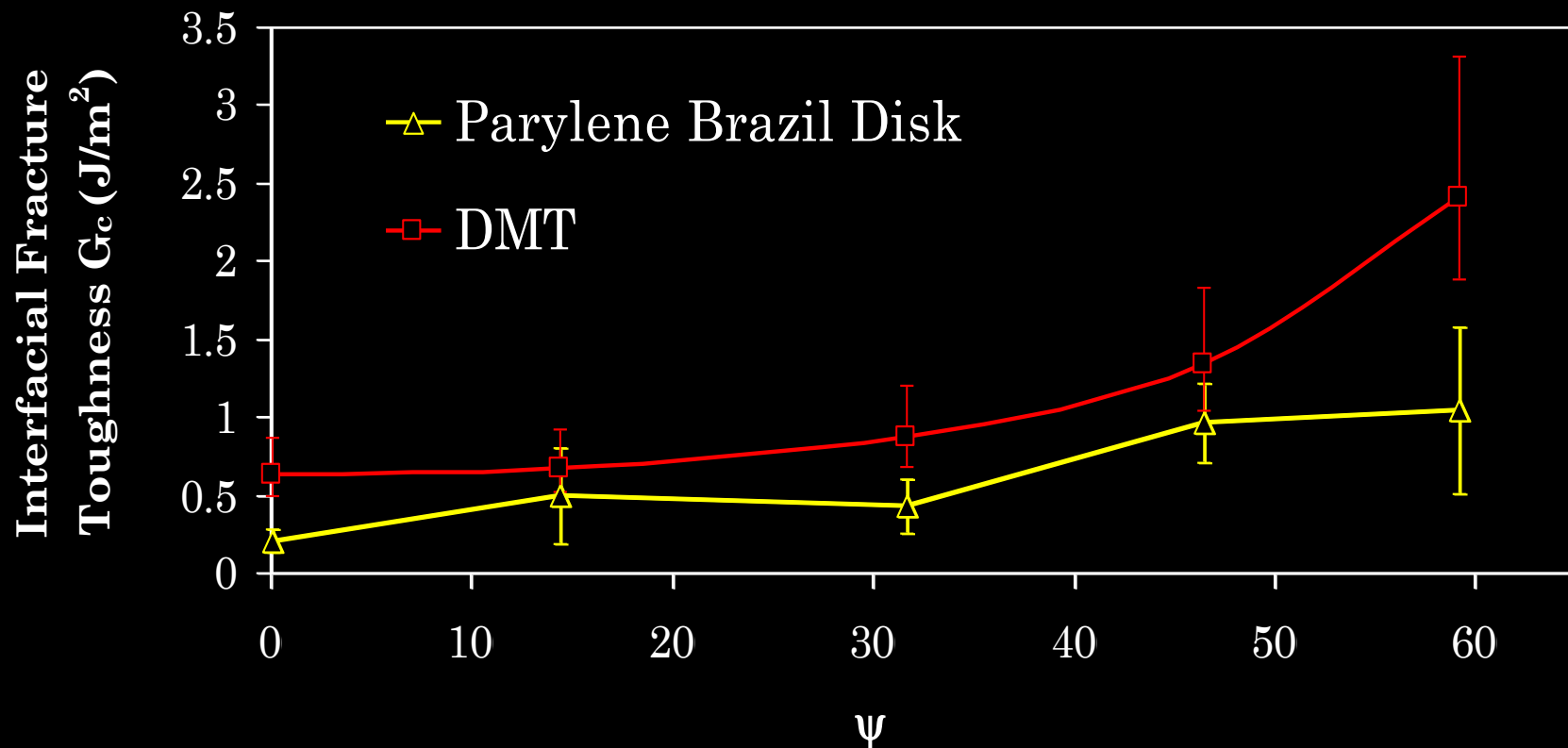
● **Glue:**
Spectra
found
Mainly C
and O
(Indicative
of GLUE)

● **Steel:**
Spectra
found
> 27% Fe
(Indicative
of steel)

Comparison of DMT models and Interfacial Fracture Experiments

$$F_{DMT} = 2\pi\gamma\mathcal{R}$$

$$G = G_0(1 + \tan^2 \Psi)$$





Atkinson Model

- *Atkinson et al. (1982)*

$$N_I = (K_I)/\sigma_0\sqrt{\pi a}, \quad N_{II} = (K_{II})/\sigma_0\sqrt{\pi a}$$

$$\sigma_0 = P/\pi l.$$

$$N_I = \sum_{i=1}^n T_i \left(\frac{a}{l}\right)^{2i-2} A_i(\theta), \quad N_{II} = 2 \sin 2\theta \sum_{i=1}^n S_i \left(\frac{a}{l}\right)^{2i-2} B_i(\theta)$$

A_i and B_i are coefficients related to θ

$$\hat{\psi} = \tan^{-1} \frac{K_{II}}{K_I} + \omega + d \ln\left(\frac{\hat{L}}{h}\right)$$

$$G = G_I + G_{II} = \frac{K_I^2 + K_{II}^2}{E_1} = (N_I^2 + N_{II}^2) \frac{P^2}{E_1 a}$$



Fundamental Mechanism of Interfacial Fracture



- *Evans and Hutchinson (1982) presented the row model*

$$\frac{\Delta G}{G} \equiv \Sigma(\phi, \beta, \psi, \epsilon)$$

$$= + 2h \frac{[(\sin \beta + \cos \beta \tan \psi)(\sin(\beta - \phi) + \cos(\beta - \phi) \tan \psi)]}{\cos \phi (1 + \tan^2 \psi)}$$

$$- \frac{h^2 (\sin \beta + \cos \beta \tan \psi)^2}{\cos^2 \phi (1 + \tan^2 \psi)}$$

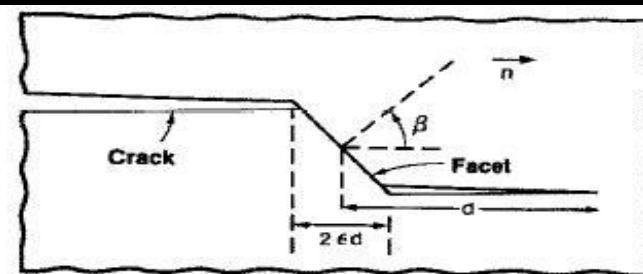
$$\phi + \psi < \pi/2,$$

$$\langle \Delta G \rangle / G = \frac{1}{\pi} \int_{\pi - \psi}^{\pi} \Sigma d\beta$$

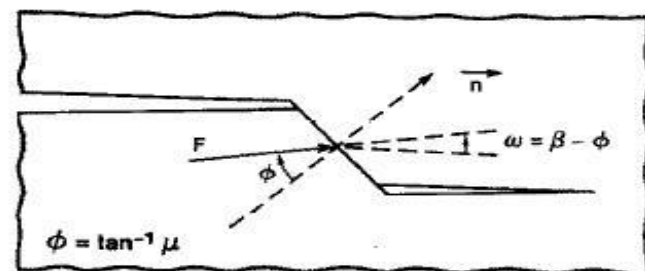
$$\phi + \psi > \pi/2$$

$$\langle \Delta G \rangle / G = \frac{1}{\pi} \int_{\pi - \psi}^{3\pi/2 - \phi - \psi} \Sigma d\beta$$

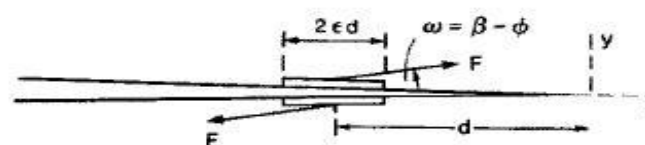
$$+ \left(\frac{\phi + \psi}{\pi} - \frac{1}{2} \right) (1 - \Omega).$$



a) Basic Configuration



b) Frictional Force



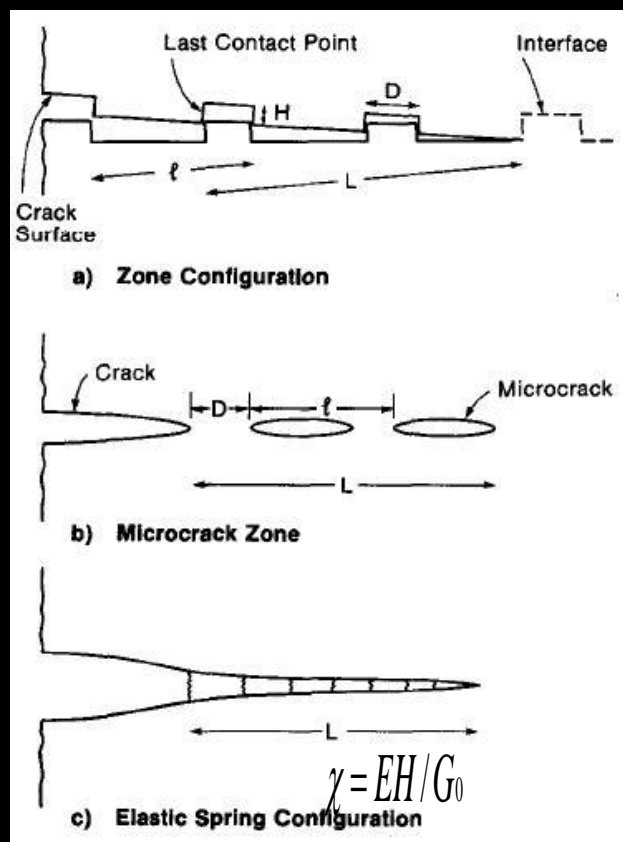
c) Elasticity Model



Fundamental Mechanism of Interfacial Fracture



- A zone model was proposed for improvement



$$\alpha = \frac{(L/l)}{\ln[1/\sin(\pi D/2l)]}$$

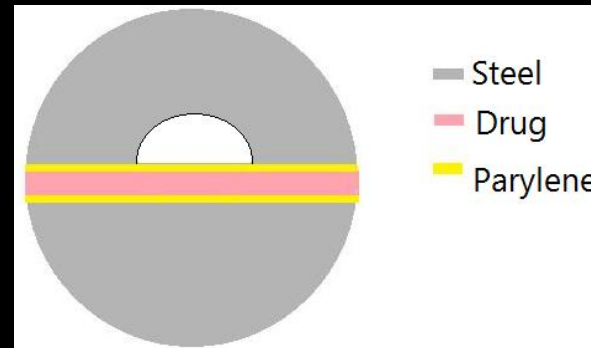
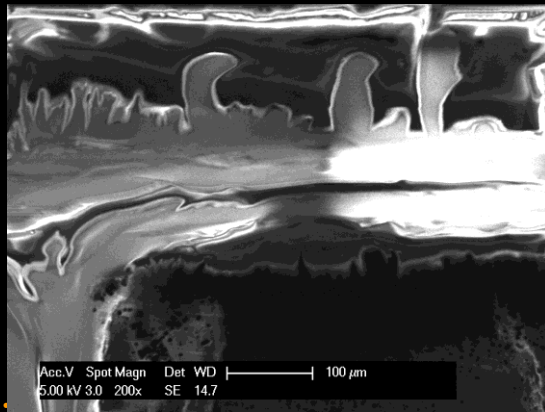
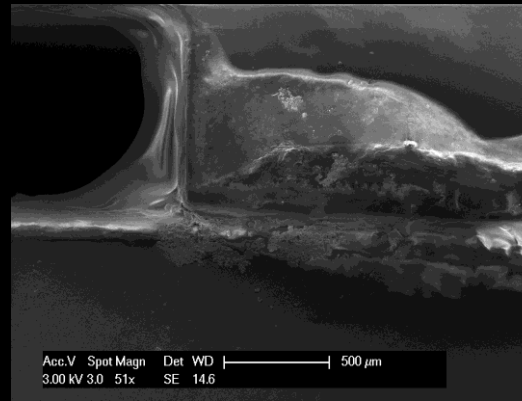
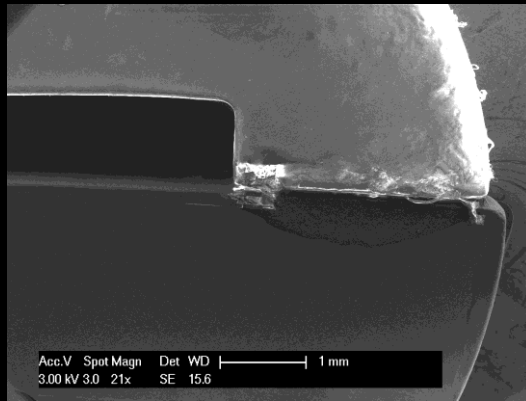
$$\alpha_0 = \frac{\pi(EH^2/lG_0)}{32(1-v^2)\ln[1/\sin(\pi D/2l)]}$$

$$\Delta G/G = \frac{\tan^2 \psi \{1 - k[\alpha_0(1 + \tan^2 \psi)(\Delta G/G + 1)]\}}{1 + \tan^2 \psi}$$

$$G_i = G_0(1 + \tan^2 \psi).$$



Crack Surface Profile Measurement



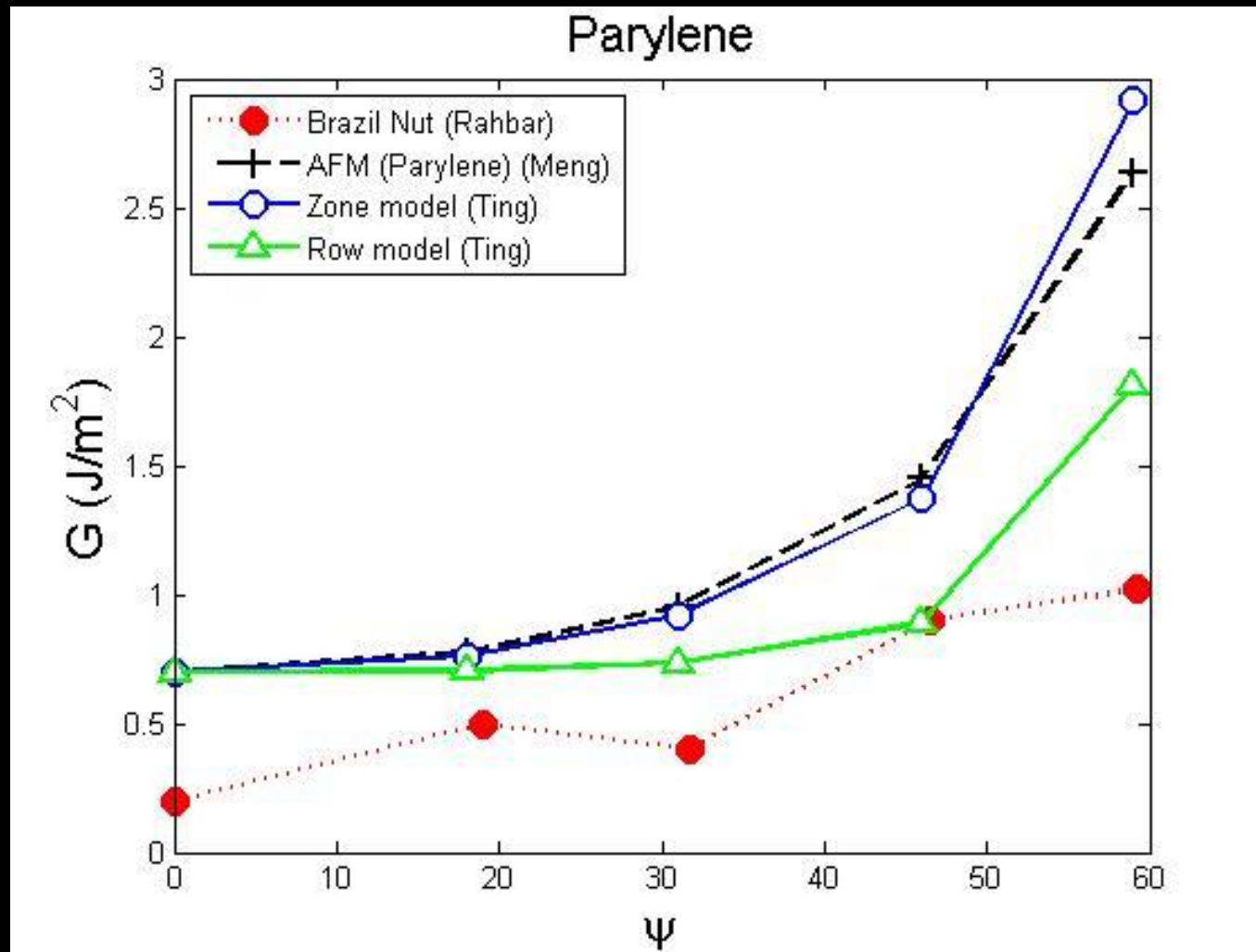
Material and Geometrical Parameters



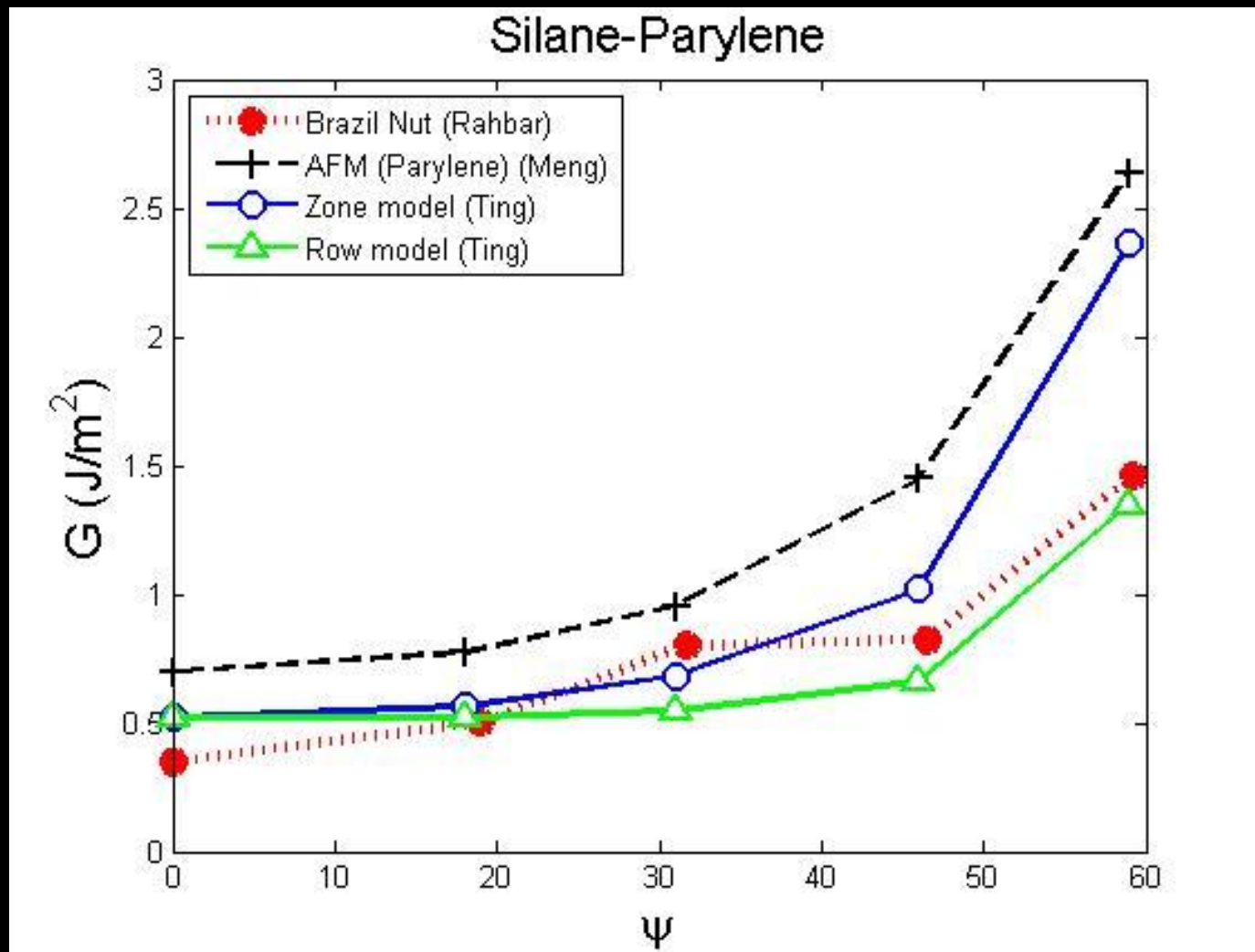
<i>Stainless Steel</i>	<i>Interface</i>	<i>Parylene</i>	<i>Interface</i>	<i>Drug</i>
$E=205\text{GPa}$		$E=3\text{GPa}$		$E=2.1\sim 3.7\text{GPa}$
$\nu=0.3$		$\nu=0.28$		$\nu=0.27$
	$G_0=0.70\text{N/m}$		$G_0=0.19\text{N/m}$	
	$L=500\mu\text{m}$		$L=1500\mu\text{m}$	
	$l=100\mu\text{m}$		$l=50\mu\text{m}$	
	$D=20\mu\text{m}$		$D=6\mu\text{m}$	
	$H=10\mu\text{m}$		$H=3\mu\text{m}$	



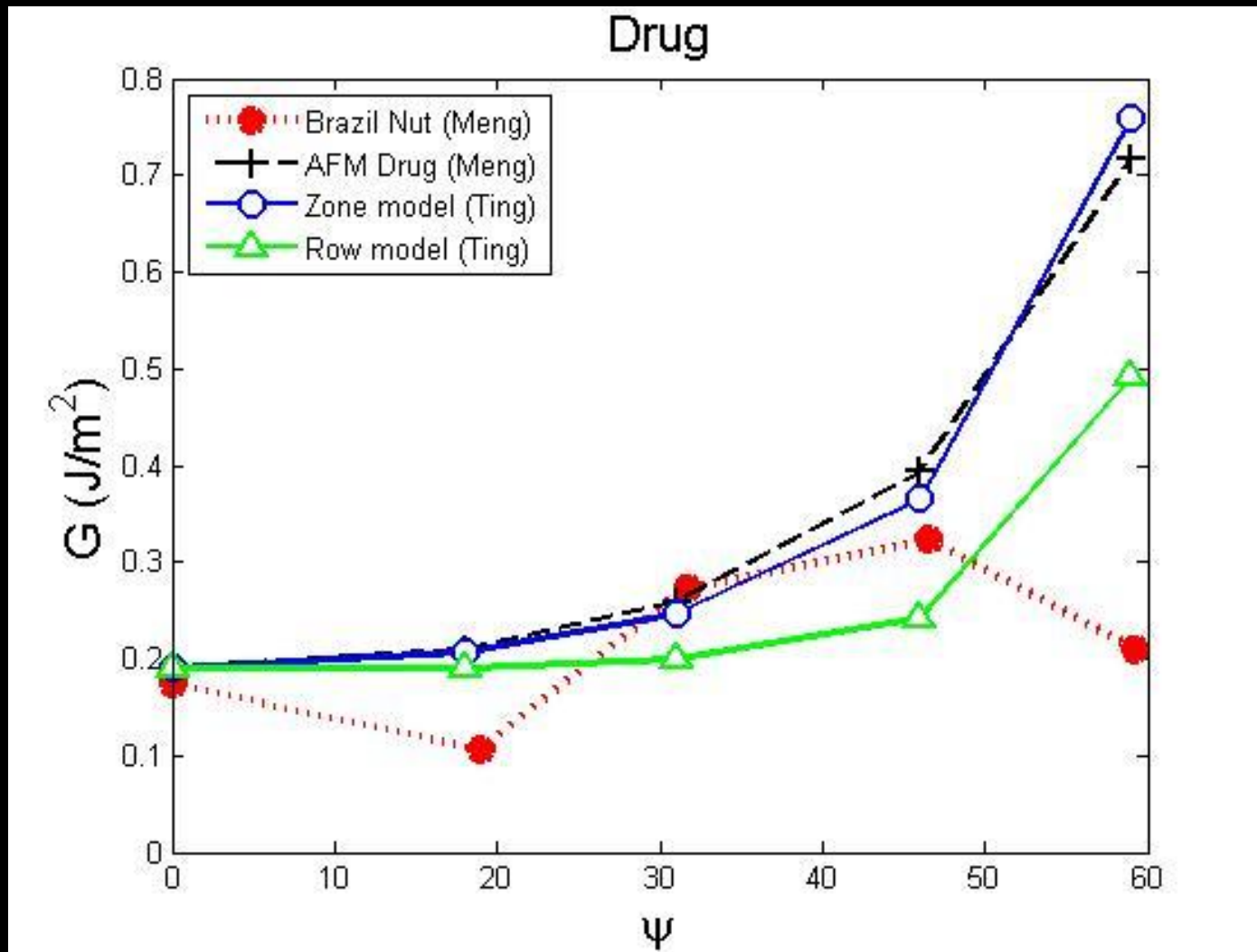
Comparison of Model Predictions



Comparison of Model Predictions



Comparison of Model Predictions



Summary and Concluding Remarks

- *This class presents some examples of the applications of adhesion and fracture mechanics concepts to drug eluting stents*
- *Pull-off forces determined from AFM experiments on bi-material pairs (useful for ranking interfaces)*
- *Brazil disk specimens used to measure mode mixity dependence of interfacial fracture toughness*
- *Link established between molecular AFM measurements of pull-off force and surface energy*
- *The surface energy estimates are in good agreement with results from Brazil disk tests*
- *Trends of mode mixity fracture toughness from row/zone models in agreement with experiments*



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- *Nima Rahbar*
- *Juan Meng*
- *Wanliang Shan*



Overview of Course

- *Introduction to fatigue crack initiation and propagation*
- *Empirical fatigue models*
- *Fundamentals of fracture mechanics*
- *Toughening mechanisms*
- *Fundamentals of fracture – brittle / ductile and mechanisms in different classes of materials*
- *Frontiers of fracture mechanics – dental multilayers and biomedical stents*

